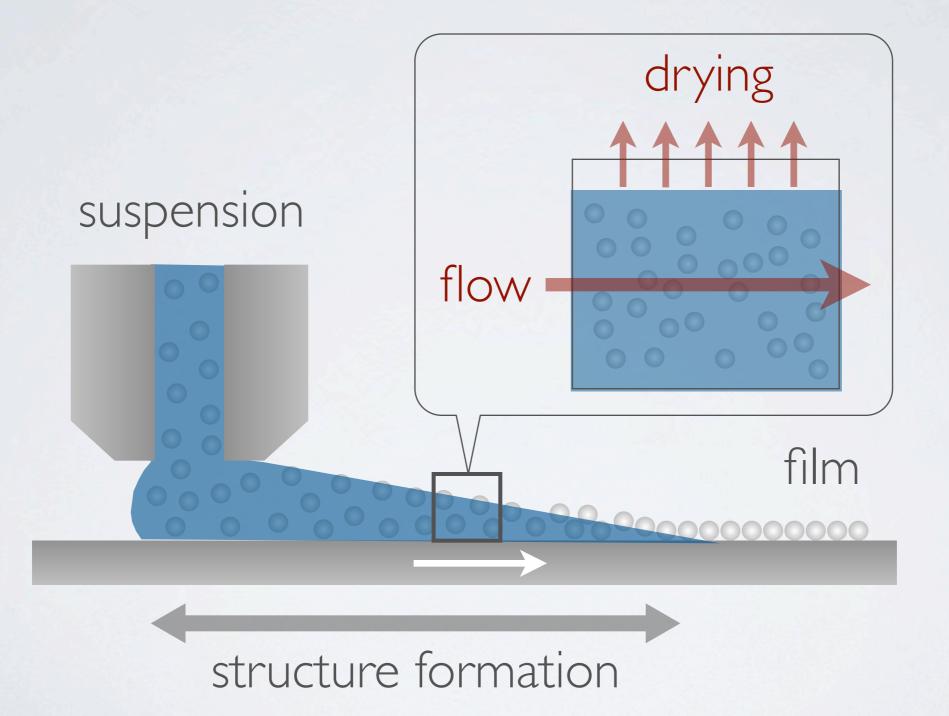
SIMULATION MODEL OF DRYING COLLOIDAL SUSPENSION ON SUBSTRATE

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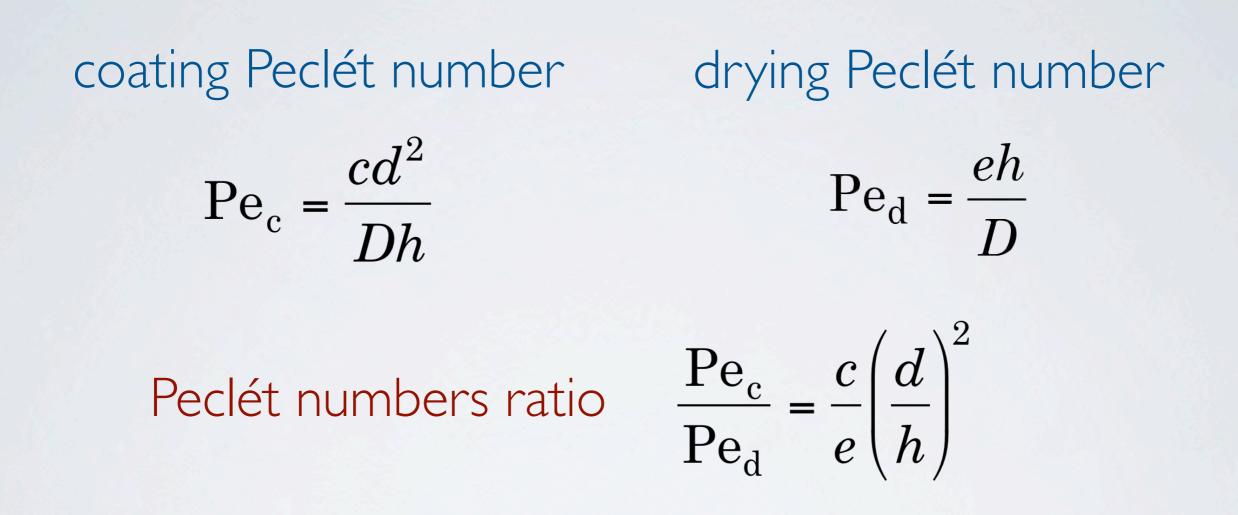
OUTLINE

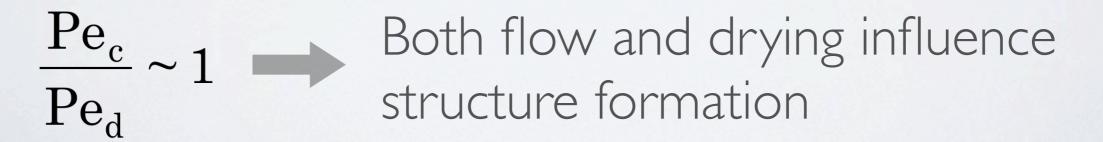
Continuous coating of colloidal suspension on substrate
Direct simulation model for drying colloidal suspension
Demonstration of present simulation model

CONTINUOUS COATING ON SUBSTRATE



PECLÉT NUMBERS





OBJECTIVES OF THIS STUDY

- Develop direct simulation model for drying colloidal suspension
- Perform flow simulations of colloidal suspension on sliding substrate with drying of solvent
 - Quantify coating-drying dynamics
 - structure of particles
 - variable drying rate

DIRECT SIMULATION MODEL

- Solves gas-liquid two phase flow on lattice using VOF (volume of fluid) method
- Solves translational/rotational motion of particles subject to contact, DLVO, capillary interactions
- Couples motion of particles with flow of solvent using immersed boundary method

Interparticle hydrodynamic interaction is included without analytical model

EQUATIONS OF FLUID MOTION

fluctuating stress

$$\rho \frac{\partial \boldsymbol{v}}{\partial t} + \rho \boldsymbol{v} \cdot \nabla \boldsymbol{v} = -\nabla p - \frac{2}{3} \nabla \cdot \left\{ \mu (\nabla \cdot \boldsymbol{v}) \boldsymbol{I} \right\} + \nabla \cdot \mu \{ \nabla \boldsymbol{v} + (\nabla \boldsymbol{v})^T \} + \nabla \cdot \boldsymbol{S} + \Phi \alpha$$

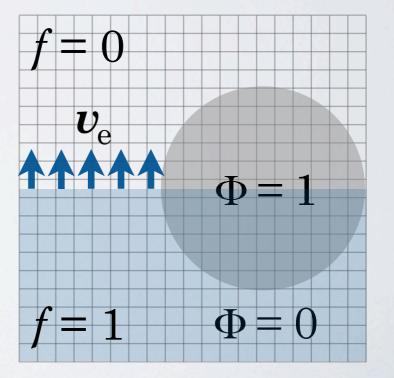
acceleration

$$\alpha = \rho \frac{\boldsymbol{v}^{P} - \boldsymbol{v}}{\Delta t} + \rho \boldsymbol{v} \cdot \nabla \boldsymbol{v} + \nabla \boldsymbol{p} + \frac{2}{3} \nabla \cdot \left\{ \mu (\nabla \cdot \boldsymbol{v}) \boldsymbol{I} \right\} - \nabla \cdot \mu \{ \nabla \boldsymbol{v} + (\nabla \boldsymbol{v})^{T} \} - \nabla \cdot \boldsymbol{S}$$

$$\rho = f \rho_{\rm l} + (1-f) \rho_{\rm g} \,, \quad \mu = f \mu_{\rm l} + (1-f) \mu_{\rm g} \,$$

$$\frac{\partial f}{\partial t} + (\boldsymbol{v} + \boldsymbol{v}_{e}) \cdot \nabla f = 0 \qquad \nabla \cdot \boldsymbol{v} = \frac{\rho_{1} - \rho_{g}}{\rho} \boldsymbol{v}_{e} \cdot \nabla f$$

local drying velocity



EQUATIONS OF PARTICLE MOTION

$$m\frac{d\boldsymbol{v}}{dt} = \boldsymbol{F}^{\rm co} + \boldsymbol{F}^{\rm D} + \boldsymbol{F}^{\rm ca} + \boldsymbol{F}^{\rm h}$$

$$\int I \frac{d\omega}{dt} = T^{\rm co} + T^{\rm h}$$

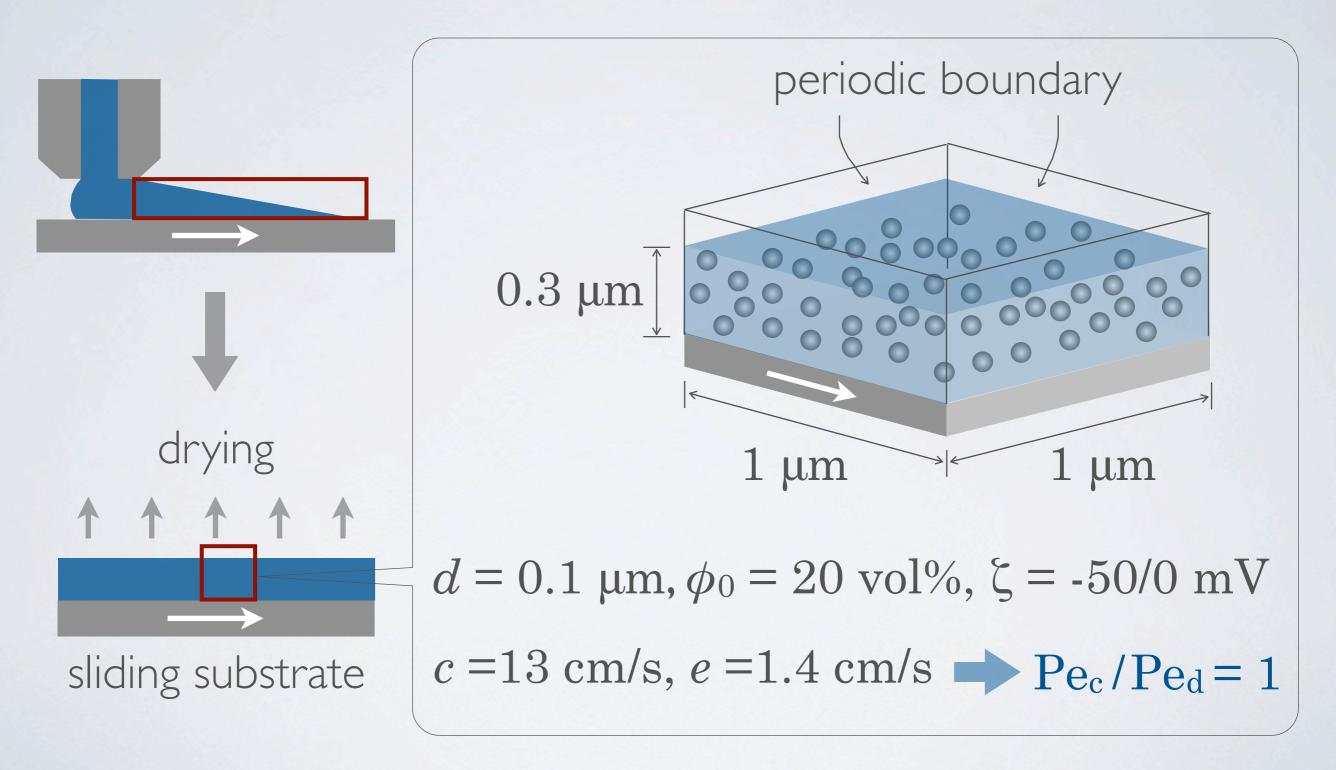
$$F^{h} = -\int \rho \Phi \alpha dr$$

$$V_{p} \quad \text{acceleration}$$

$$T^{h} = -\int (r \times \rho \Phi \alpha) dr$$

$$V_{p} \quad \text{acceleration}$$

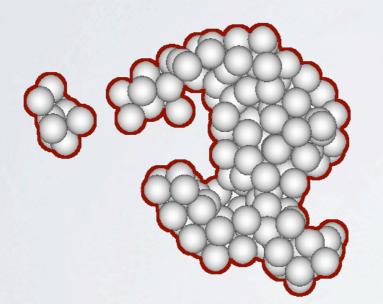
SIMULATION CONDITION



QUANTIFICATION OF STRUCTURE

Non-dimensional Boundary Area (NBA)

 $NBA = \frac{\text{surface area of aggregates}}{\text{total surface area of particles}} = \frac{1}{12N} \sum_{k=0}^{12} \left\{ \left(12 - k\right)n(k) \right\}$



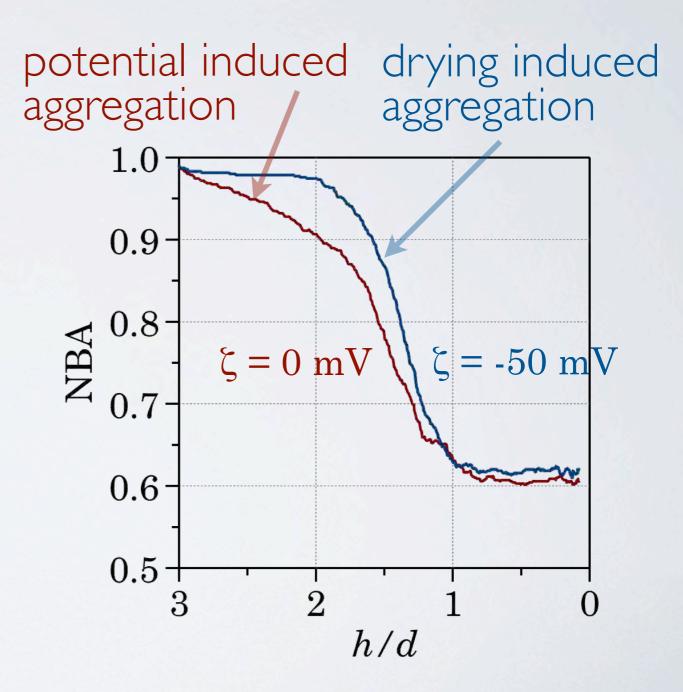
k : coordinate number n(k) : number of particles with coordinate number of kN : total number of particles

NBA=0 : 3D hexagonal close-packed NBA=0.5 : 2D hexagonal close-packed NBA=1 : complete-dispersed

STRUCTURE OF PARTICLES

 $\zeta = -50 \text{ mV}$

NBA vs interface height



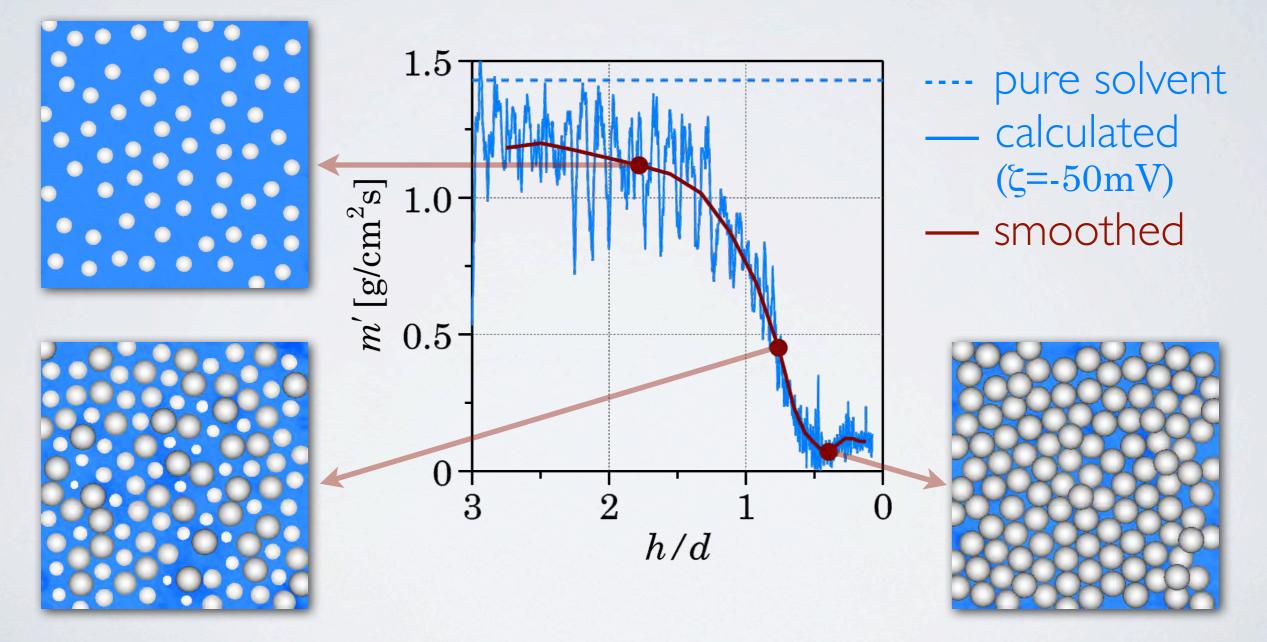
plan

side

The 3rd Asian Coating Workshop, 2011.7.4-5

VARIABLE DRYING RATE

drying rate vs interface height



CONCLUSION

- Developed direct simulation model for drying colloidal suspension
- Quantify structure formation of particles using NBA
- Quantify variable drying rate in which constant rate of drying changes to decreasing rate of drying.